

Estimated distributions of low flow characteristic – some remarks about their instabilities

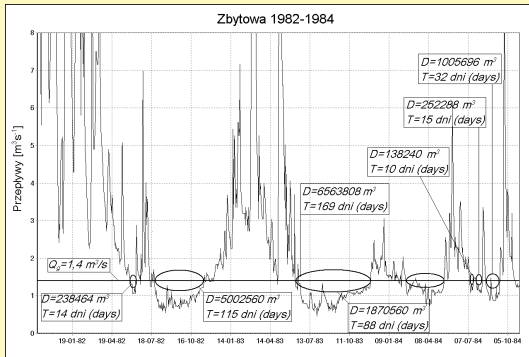
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on Low Flows and Droughts
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POT method



For given threshold level Q_g define three low flow characteristics:

- 1 Deficit in [m^3]

$$D_\tau = \int_{t_p}^{t_k} (Q_g - Q(t)) dt$$

- 2 Duration [days]

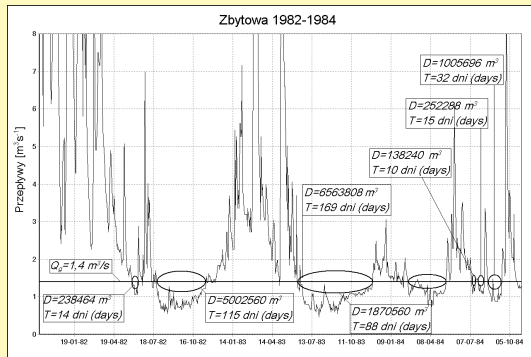
$$T_\tau = t_k - t_p + 1,$$

$$\tau = 1, 2, \dots$$

- 3 Minimal outflow P_τ



POT method, example

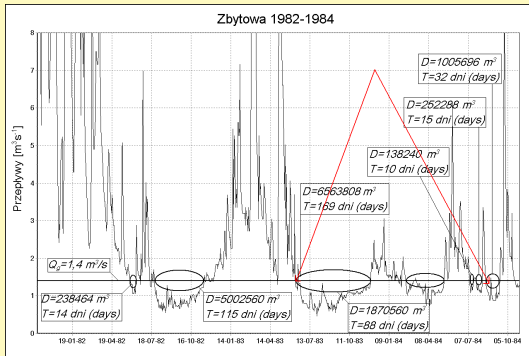


For observed low flows the additional restrictions are imposed [Zelenhaisić and Salvai 1987]:

- Minimum duration m_t ;
- Minimum interval between successive low flows m_d ;
- Coefficient α setting a minimum deficiency.



POT method, example



Threshold level $Q_g = Q_{70\%}$

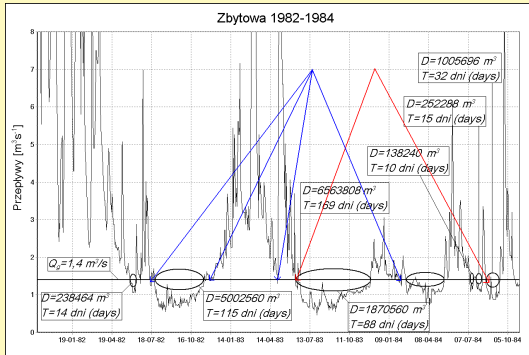
Minimum duration 5 days.

Minimum interval between successive low flows 3 days.

Coefficient: $\alpha = 0,03$.



POT method, example



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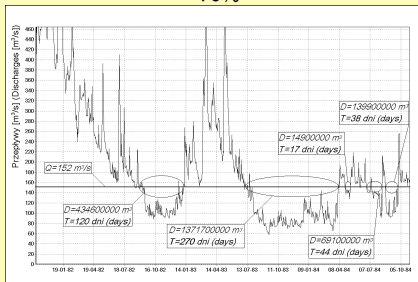
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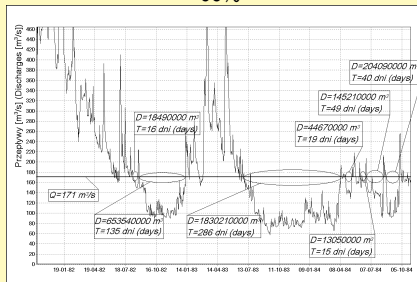
POT method, modification of Q_g

Cigacice 1982 - 84

$Q_{70\%}$



$Q_{60\%}$



$$\Pr(D \leq 1371.7 \text{ millions m}^3 | Q_{70\%}) \leftrightarrow \Pr(D \leq 1830.21 \text{ millions m}^3 | Q_{60\%})$$

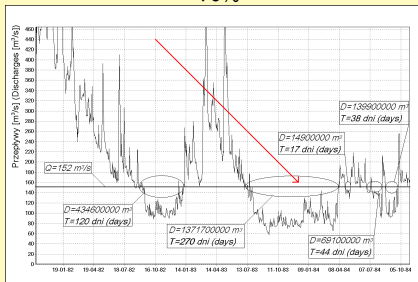
$$\Pr(T \leq 270 \text{ days} | Q_{70\%}) \leftrightarrow \Pr(T \leq 286 \text{ days} | Q_{60\%})$$



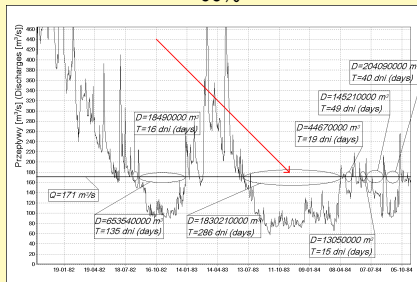
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The standard approach

Low flow is a period in which the flows are equal to or lower than the accepted threshold Q_g . When determining the flow boundary one can use various criteria. Some of them can be hydrological, other economical or ecological. They should depend on the purpose of developing.

Normally:

- Q_g is equal to the highest minimum annual flow;
- $Q_g = Q_{70\%}$ or $Q_g = Q_{90\%}$.

No one looks at the statistical implications of this approach.



Distributions

Assumptions:

- For given Q_g the low flow deficit or duration are having:
 - GEV distribution:

$$F(x) = \exp \left\{ - \left[1 + \xi \left(\frac{x - \mu}{\sigma} \right) \right]^{-\frac{1}{\xi}} \right\}, \quad x > \mu - \frac{\sigma}{\xi}$$

- log-normal distribution:

$$F(x) = \int_0^x \frac{1}{\sqrt{2\pi\sigma t}} \exp \left(-\frac{(\ln t - \mu)^2}{2\sigma^2} \right) dt$$

unknown parameters: μ, σ, ξ or μ, σ are estimated by maximum likelihood method.



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- $Q_{90\%} \leq Q_g \leq Q_{55\%}$ – step Q_g corresponds to the accuracy of flow measurement in the watershed profile.



Tested watershed profiles

Profiles:

- ① Kuripapango (Ngaruroro) (1965-2000)
- ② Bogusław (Prosna) (lowland) (1965 - 2005)
- ③ Bystrzyca Kłodzka (Nysie Kłodzka) (mountains) ¹ (1965 - 2005)

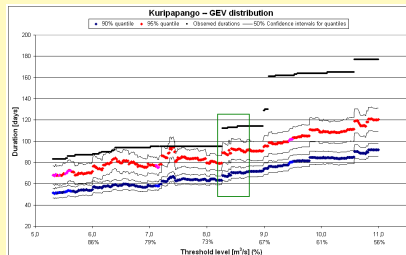
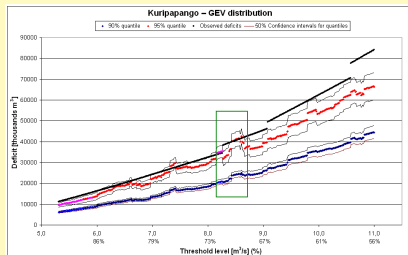
Zelenhaisić and Salvai restrictions:

- Minimum duration $m_t = 5$ days;
- Minimum interval between successive low flows $m_d = 3$ days;
- Setting a minimum deficiency coefficient $\alpha = 0,09$ for Kuropapango and $\alpha = 0,03$ for Bogusław and Bystrzyca Kłodzka.

¹Polish data were provided by Polish Institute of Meteorology and Water Management



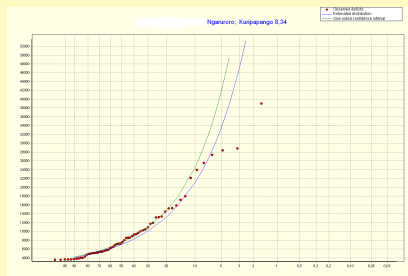
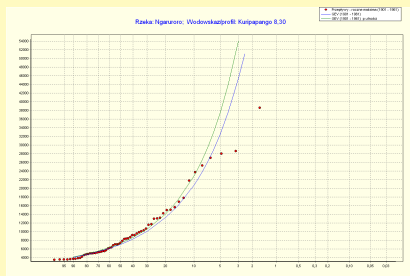
Kuripapango



$$Q_{g1} = 8,30 \text{ m}^3/\text{s}; \quad Q_{g2} = 8,34 \text{ m}^3/\text{s}; \quad \frac{Q_{g2} - Q_{g1}}{Q_{g1}} \approx 0,5\%$$



Kuripapango

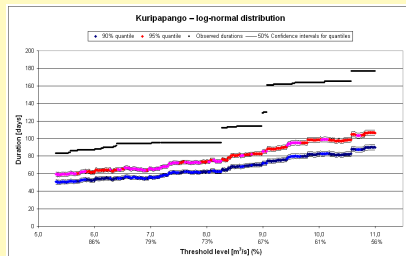
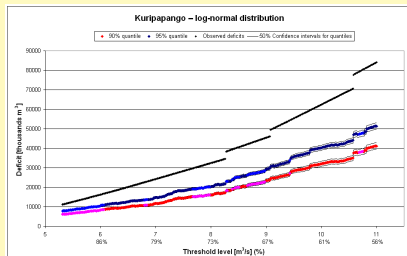


$p = 0,90$	$D_{8,30} = 20756;$	$D_{8,34} = 21065$	$c_1 = 1,5\%$
$p = 0,95$	$D_{8,30} = 32535;$	$D_{8,34} = 33436$	$c_2 = 2,7\%$
$p = 0,99$	$D_{8,30} = 93171;$	$D_{8,34} = 98942$	$c_3 = 6,2\%$

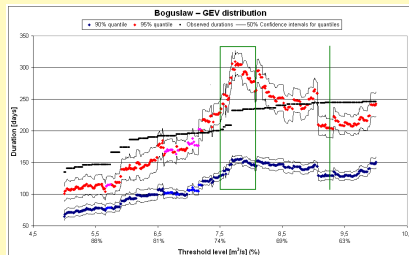
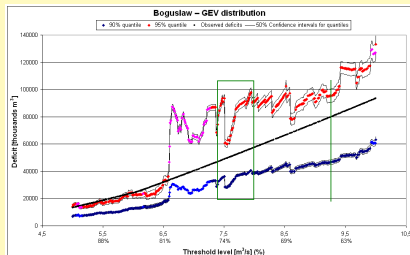
D in thousands m^3/s



Kuripapango



Bogusław

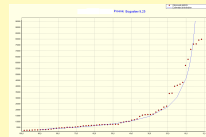
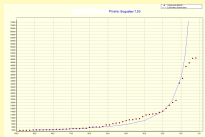


$$Q_{g1} = 7,94; \quad Q_{g2} = 7,56; \quad Q_{g3} = 7,5; \quad Q_{g4} = 9,25 m^3/s$$

$$d_1 = \frac{Q_{g2} - Q_{g1}}{Q_{g1}} \approx 4,8\% \quad d_2 = \frac{Q_{g3} - Q_{g2}}{Q_{g2}} \approx 0,8\% \quad d_3 = \frac{Q_{g4} - Q_{g2}}{Q_{g2}} \approx 22,4\%$$



Bogusław

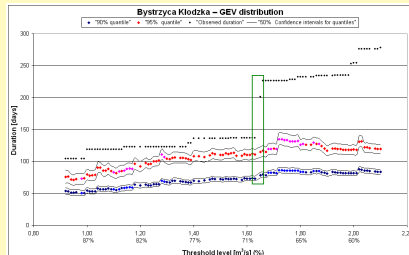
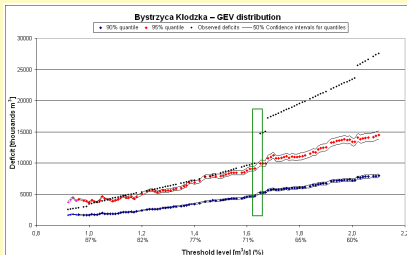


$d_1 = 4,8\%$	$p = 0,90$	$Q_{7,56} = 29096$	$Q_{7,94} = 38529;$	$c_1 = 24,5\%$
	$p = 0,95$	$Q_{7,56} = 62854$	$Q_{7,94} = 90407;$	$c_1 = 30,5\%$
	$p = 0,99$	$Q_{7,56} = 371258$	$Q_{7,94} = 644834;$	$c_1 = 42,4\%$
$d_2 = 0,8\%$	$p = 0,90$	$Q_{7,50} = 36283;$	$Q_{7,56} = 29096$	$c_1 = 24,7\%$
	$p = 0,95$	$Q_{7,50} = 93592;$	$Q_{7,56} = 62854$	$c_1 = 48,9\%$
	$p = 0,99$	$Q_{7,50} = 839337;$	$Q_{7,56} = 371258$	$c_1 = 126,1\%$
$d_3 = 22,4\%$	$p = 0,90$	$Q_{7,56} = 29096;$	$Q_{9,25} = 46671$	$c_1 = 60,4\%$
	$p = 0,95$	$Q_{7,56} = 62854;$	$Q_{9,25} = 95431$	$c_1 = 51,8\%$
	$p = 0,99$	$Q_{7,56} = 371258;$	$Q_{9,25} = 493177$	$c_1 = 32,8\%$

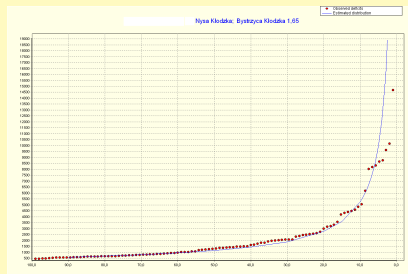
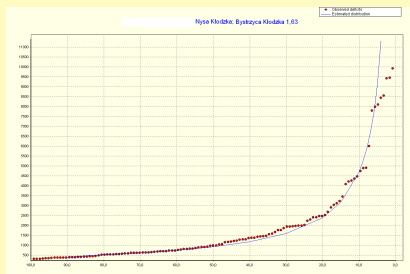
D in thousands m^3/s



Bystrzyca Kłodzka



Bystrzyca Kłodzka



$$Q_{g1} = 1,65; \quad Q_{g2} = 1,63$$

$$c_1 = \frac{Q_{g2} - Q_{g1}}{Q_{g1}} \approx 1,2\%$$

$$p = 0,90 \quad c_1 = 11,7\%$$

$$p = 0,95 \quad c_2 = 8,9\%$$

$$p = 0,99 \quad c_3 = 4,3\%$$



Research questions

What are the causes of instability?

Are they the result of numerical, statistical
calculations,
or are the property of the catchment?

Thank you for your attention.

